

COFL

Patent No.: 6895081B1

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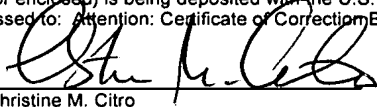
Atty. Docket No.: T0529.70015US00  
(PATENT)



IN THE UNITED STATES PATENT AND TRADEMARK OFFICE

Applicant: Kurt E. Schmidt et al.  
Serial No.: 09/294,563  
Confirmation No.: 6271  
Filed: April 20, 1999  
Patent No.: 6895081B1  
For: PREDICTING PERFORMANCE OF TELEPHONE LINES FOR  
DATA SERVICES

Examiner: N/A  
Art Unit: N/A

<b>Certificate of Mailing Under 37 CFR 1.8(a)</b>	
I hereby certify that this paper (along with any paper referred to as being attached or enclosed) is being deposited with the U.S. Postal Service on the date shown below with sufficient postage as First Class Mail, in an envelope addressed to: Attention: Certificate of Correction Branch, Commissioner for Patents, P.O. Box 1450, Alexandria, VA 22313-1450.	
Dated: 7/23/07	 Christine M. Citro

Attention: Certificate of Correction Branch  
Commissioner for Patents  
P.O. Box 1450  
Alexandria, VA 22313-1450

**Certificate**

JUL 30 2007

**of Correction**

Dear Sir:

**REQUEST FOR CERTIFICATE OF CORRECTION  
PURSUANT TO 37 CFR 1.322**

Upon reviewing the above-identified patent, Patentee noted errors in the printed patent, which Patentee respectfully requests should be corrected.

Specifically, Appendix 1 and Appendix 2 referenced in the specification and included with the application as filed were not printed with the issued patent.

To demonstrate that the error and the correction are apparent from the application file, enclosed is a copy of Appendix 1 and Appendix 2 filed with the application. A copy of the transmittal letter for the application indicating that Appendix 1 and Appendix 2 were included with the application is also included. Further, Appendix 1 is referenced in the application as filed and in

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the printed patent at Column 4, line 62 and Appendix 2 is referenced in the application as filed in Column 5, line 67 and Column 6, line 1.

The enclosed papers from the prosecution history demonstrate that the information classified as Appendix 1 and Appendix 2, though not printed with the issued patent, were filed with the application.

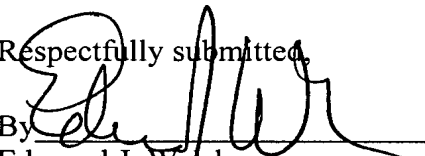
The requested changes to the printed patent make clear that Appendix 1 and Appendix 2 form a portion of patent 6,895,081 B1. This change does not constitute new matter because the information to be added by this certificate was included with the application as filed. Therefore, no fee is required.

Transmitted herewith is a proposed Certificate of Correction effecting such amendment. Patentee respectfully solicits the granting of the requested Certificate of Correction.

Should any questions arise concerning the foregoing, please contact the undersigned at the telephone number listed below.

The Director is hereby authorized to charge any deficiency in the fees filed, asserted to be filed or which should have been filed herewith (or with any paper hereafter filed in this application by this firm) to our Deposit Account No. 23/2825, under Docket No. T0529.70015US00. A duplicate copy of this paper is enclosed.

Dated: July 23, 2007

Respectfully submitted,  
  
By Edmund J. Walsh  
Registration No.: 32,950  
WOLF, GREENFIELD & SACKS, P.C.  
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# UNITED STATES PATENT AND TRADEMARK OFFICE

## CERTIFICATE OF CORRECTION

Page 1 of 4

PATENT NO. : 6895081B1  
 APPLICATION NO. : 09/294,563  
 ISSUE DATE : May 17, 2005  
 INVENTOR(S) : Kurt E. Schmidt, David J. Groessl and Yun Zhang

It is certified that an error appears or errors appear in the above-identified patent and that said Letters Patent is hereby corrected as shown below:

### In the Specification:

In column 4, line 62, delete "Appendix" and insert therefore --Table--

In column 5, before line 1 insert:

-- Table 1

$f_i$ :

150, 600, 1050, 1500, 1950, 2400, 2850, 3300, 3750, 4200, 4650, 5100, 5550, 6000, 6450, 6900, 7350, 7800, 8250, 8700, 9150, 9600, 10050, 10500, 10950, 11400, 11850, 12300, 12750, 13200, 13650, 14100, 14550, 15000, 15450, 15900, 16350, 16800, 17250, 17700, 18150, 18600, 19050, 19500, 19950.

$N$ :

1, 4, 7, 10, 13, 16, 19, 22, 25, 28, 31, 34, 37, 40, 43, 46, 49, 52, 55, 58, 61, 64, 67, 70, 73, 76, 79, 82, 85, 88, 91, 94, 97, 100, 103, 106, 109, 112, 115, 118, 121, 124, 127, 130, 133 respectively.

$\Phi_i$ :

5.9738, 1.3564, 2.4683, 4.8575, 4.7434, 2.2972, 4.6015, 1.9156, 2.5660, 4.5986, 4.6452, 3.4542, 3.6341, 0.8848, 4.3410, 2.1606, 4.2342, 4.2147, 3.1058, 5.909, 5.2782, 5.1159, 5.4354, 5.6124, 0.5751, 3.8940, 3.3812, 6.0230, 2.3239, 2.7284, 4.8032, 4.1488, 2.3427, 4.6362, 0.9163, 2.9335, 1.0363, 2.3272, 3.2040, 4.0025, 2.0028, 5.8444, 2.4525, 1.4760, 1.1770--

MAILING ADDRESS OF SENDER (Please do not use customer number below):

**6,895,081B1**

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In column 5, line 67 delete "Appendix" and insert therefore --Table--.

In column 6, line 1 delete "Appendix" and insert therefore --Table--.

In column 6, following line 3, insert:

--Table 2

**30Hz Raw Measurements:**

Ytr(30) – Admittance tip-to-ring measured at 30Hz

Ytg(30) – Admittance tip-to-ground measured at 30Hz

Yrg(30) – Admittance ring-to-ground measured at 30Hz

**30Hz Derived Measurements:**

30Gtr – Conductance tip-to-ring measured at 30Hz =  $\text{real}(\text{Ytr}(30))$

30Str – Susceptance tip-to-ring measured at 30Hz =  $\text{imag}(\text{Ytr}(30))$

30Gtg – Conductance tip-to-ground measured at 30Hz =  $\text{real}(\text{Ytg}(30))$

30Stg – Susceptance tip-to-ground measured at 30Hz =  $\text{imag}(\text{Yt}(30))$

30Ctr – Capacitance tip-to-ring measured at 30Hz =  $\text{Str}(30)/(2 \cdot \pi \cdot 30)$

30Ctg – Capacitance tip-to-ground measured at 30Hz =  $\text{St}(30)/(2 \cdot \pi \cdot 30)$

Lmeas – Length in kft measured at 30Hz =  $30\text{Ctg}/17.47$

**150Hz-20KHz Raw Measurements:**

Ytr(f) – Admittance tip-to-ring where  $f=150\text{Hz}, 600\text{Hz}, 1050\text{Hz}, 1500\text{Hz}, \dots, 19950\text{Hz}$

Ytg(f) – Admittance tip-to-ground where  $f=150\text{Hz}, 600\text{Hz}, 1050\text{Hz}, 1500\text{Hz}, \dots, 19950\text{Hz}$

Yrg(f) – Admittance ring-to-ground where  $f=150\text{Hz}, 600\text{Hz}, 1050\text{Hz}, 1500\text{Hz}, \dots, 19950\text{Hz}$

**150Hz-20KHz Derived Measurements:**

150Gtr – Conductance tip-to-ring measured at 150Hz =  $\text{real}(\text{Ytr}(150))$

600Gtr – Conductance tip-to-ring measured at 600Hz =  $\text{real}(\text{Ytr}(600))$

19950Gtr – Conductance tip-to-ring measured at 19950Hz =  $\text{real}(\text{Ytr}(19950))$

150Str – Susceptance tip-to-ring measured at 150Hz =  $\text{imag}(\text{Ytr}(150))$

600Str – Susceptance tip-to-ring measured at 600Hz =  $\text{imag}(\text{Ytr}(600))$

19950Str – Susceptance tip-to-ring measured at 19950Hz =  $\text{imag}(\text{Ytg}(19950))$

150Gtg – Conductance tip-to-ground measured at 150Hz =  $\text{real}(\text{Ytg}(150))$

600Gtg – Conductance tip-to-ground measured at 600Hz =  $\text{real}(\text{Ytg}(600))$

19950Gtg – Conductance tip-to-ground measured at 19950Hz =  $\text{real}(\text{Ytg}(19950))$

150Stg – Susceptance tip-to-ground measured at 150Hz =  $\text{imag}(\text{Ytg}(150))$

600Stg – Susceptance tip-to-ground measured at 600Hz =  $\text{imag}(\text{Ytg}(600))$

19950Stg – Susceptance tip-to-ground measured at 19950Hz =  $\text{imag}(\text{Ytg}(19950))$

150Ctr – Capacitance tip-to-ring measured at 150Hz =  $150\text{Str}/(2 \cdot \pi \cdot 150)$

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600 Ctr – Capacitance tip-to-ring measured at 600Hz =  $600\text{Str}/(2*\pi*600)$

19950Ctr – Capacitance tip-to-ring measured at 19950Hz =  $9950\text{Str}/(2*\pi*19950)$

150Ctg – Capacitance tip-to-ground measured at 150Hz =  $150\text{Stg}/(2*\pi*150)$

600Ctg – Capacitance tip-to-ground measured at 600Hz =  $600\text{Stg}/(2*\pi*600)$

19950Ctg – Capacitance tip-to-ground measured at 19950Hz =  $19950\text{Stg}/(2*\pi*19950)$

#### 150Hz-20KHz Secondary Derived Measurements:

C30/C4K – Ratio of tip-to-ground Capacitance at 30Hz to 4200Hz

C4K/C10K – Ratio of tip-to-ground Capacitance at 4200Hz to 10050Hz

Cslope – Tip-to-ground Capacitance ratio slope =  $(C4K/C10K)/(C30/C4K)$

C30-C4K – Difference in tip-to-ground Capacitance at 30Hz and 4200Hz

C4K-C10K – Difference in tip-to-ground Capacitance at 4200Hz and 10050Hz

Cdelta – Tip-to-ground Capacitance difference delta =  $(C4K-C10K)/(C30-C4K)$

G4K-G30 – Ratio of tip-to-ground Conductance at 4200Hz and 30Hz

G10K-G4K – Ratio in tip-to-ground Conductance at 10050Hz and 4200Hz

Gslope – Tip-to ground Conductance ratio slope =  $(G10K/G4K)/(G4K/G30)$

G4K-G30 – Difference in tip-to-ground Conductance at 30Hz and 4200Hz

G10K-G4K – Difference in tip-to-ground Conductance at 4200Hz and 10050Hz

Gdelta – Tip-to-ground Conductance difference delta =  $(G10K-G4K)/(G4K-G30)$

C30/G30 – Ratio of Tip-to-ground Capacitance to Conductance at 30Hz

C30/G4K – Ratio of Tip-to-ground Capacitance at 30Hz to Conductance at 4200Hz

C4K/G4K – Ratio of Tip-to-ground Capacitance to Conductance at 4200Hz

Gtr\_dmax – Maximum positive slope of  $Gtr(f) = \max(\text{derivative}(Gtr(f)/df))$

Gtr\_fmax – Frequency at which Gtr\_dmax occurs

Gtr\_dmin – Maximum negative slope of  $Gtr(f) = \min(\text{derivative}(Gtr(f)/df))$

Gtr\_fmin – Frequency at which Gtr\_dmin occurs

Gtr\_fpk – Frequency of first peak (local maxima) in  $Gtr(f)$

Gtr\_fval – Frequency of first valley (local minima) in  $Gtr(f)$

Gtr\_d\_delta – Gtr Max/Min Derivative difference =  $Gtr\_dmax - Gtr\_dmin$

Gtr\_pk\_delta – Gtr peak/valley frequency difference =  $Gtr\_fval - Gtr\_fpk$

Gtr\_pk – Value of  $Gtr(f)$  at frequency  $Gtr\_fpk$

Gtr\_val – Value of  $Gtr(f)$  at frequency  $Gtr\_fval$

Gtr\_delta – Gtr peak/valley difference =  $Gtr\_pk - Gtr\_val$

Gtg\_dmax – Maximum positive slope of  $Gtg(f) = \max(\text{derivative}(Gtg(f)/df))$

Gtg\_fmax – Frequency at which Gtg\_dmax occurs

Gtg\_dmin – Maximum negative slope of  $Gtg(f) = \min(\text{derivative}(Gtg(f)/df))$

Gtg\_fmin – Frequency at which Gtg\_dmin occurs

Gtg\_d\_delta – Gtg Max/Min Derivative difference =  $Gtg\_dmax - Gtg\_dmin$

Ctr\_dmax – Maximum positive slope of  $Ctr(f) = \max(\text{derivative}(Ctr(f)/df))$

Ctr\_fmax – Frequency at which Ctr\_dmax occurs

Ctr\_dmin – Maximum negative slope of  $Ctr(f) = \min(\text{derivative}(Ctr(f)/df))$

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Ctr\_fmin – Frequency at which Ctr\_dmin occurs  
 Ctr\_fpk – Frequency of first peak (local maxima) in Ctr(f)  
 Ctr\_fval – Frequency of first valley (local minima) in Ctr(f)  
 Ctr\_d\_delta – Ctr Max/Min Derivative difference = Ctr\_dmax - Ctr\_dmin  
 Ctr\_pk\_delta – Ctr peak/valley frequency difference = Ctr\_fval - Ctr\_fpk  
 Ctr\_val – Value of Ctr(f) at frequency Ctr\_fval

Ctg\_dmax – Maximum positive slope of Ctg(f) = max(derivative(Ctg(f)/df))  
 Ctg\_fmax – Frequency at which Ctg\_dmax occurs  
 Ctg\_dmin – Maximum negative slope of Ctg(f) = min(derivative(Ctg(f)/df))  
 Ctg\_fmin – Frequency at which Ctg\_dmin occurs  
 Ctg\_d\_delta – Ctg Max/Min Derivative difference = Ctg\_dmax - Ctg\_dmin

Str\_dmax – Maximum positive slope of Str(f) = max(derivative(Str(f)/df))  
 Str\_fmax – Frequency at which Str\_dmax occurs  
 Str\_dmin – Maximum negative slope of Str(f) = min(derivative(Str(f)/df))  
 Str\_fmin – Frequency at which Str\_dmin occurs

#### 150Hz-20Hz Secondary Derived Measurements:

Str\_fpk – Frequency of first peak (local maxima) in Str(f)  
 Str\_fval – Frequency of first valley (local minima) in Str(f)  
 Str\_d\_delta – Str Max/Min Derivative difference = Str\_dmax - Str\_dmin  
 Str\_pk\_delta – Str peak/valley frequency difference = Str\_fval - Str\_fpk  
 Str\_pk – Value of Str(f) at frequency Str\_fpk  
 Str\_val – Value of Str(f) at frequency Str\_fval  
 Str\_delta – Str peak/valley difference = Str\_pk - Str\_val

Stg\_dmax – Maximum positive slope of Stg(f) = max(derivative (Stg(f)/df))  
 Stg\_fmax – Frequency at which Stg\_dmax occurs  
 Stg\_dmin – Maximum negative slope of Stg(f) = min(derivative (Stg(f)/df))  
 Stg\_fmin – Frequency at which Stg\_dmin occurs  
 Stg\_fpk – Frequency of first peak (local maxima) in Stg(f)  
 Stg\_fval – Frequency of first valley (local minima) in Stg(f)  
 Stg\_d\_delta – Stg Max/Min Derivative difference = Stg\_dmax - Stg\_dmin  
 Stg\_pk\_delta – Stg peak/valley frequency difference = Stg\_fval - Stg\_fpk

Gtg20k/Gtg8k – Ratio of Gtg at 19950Hz and 8250Hz  
 Gtg20k/Gtg4k – Ratio of Gtg at 19950Hz and 4200Hz  
 Cgt30/Cgt20k – Ratio of Ctg at 30Hz and 19950Hz  
 Cgt30/Cgt8k – Ratio of Ctg at 30Hz and 8250Hz--

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# FISH & RICHARDSON P.C.

Frederick P. Fish  
1855-1930

W.K. Richardson  
1859-1951



# COPY

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Boston, Massachusetts  
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617 542-5070

Facsimile  
617 542-8906

Web Site  
www.fr.com

April 20, 1999

Attorney Docket No.: 08640/018001

## Box Patent Application

Assistant Commissioner for Patents  
Washington, DC 20231

Presented for filing is a new original patent application of:

Applicant: KURT E. SCHMIDT, DAVID J. GROESSL AND YUN ZHANG  
Title: PREDICTING PERFORMANCE OF TELEPHONE LINES FOR DATA SERVICES

Enclosed are the following papers, including those required to receive a filing date under 37 CFR §1.53(b):

	<u>Pages</u>
Specification	21
Claims	12
Abstract	1
Appendix 1	2
Appendix 2	4
Declaration	2
Drawing(s)	14

Enclosures:

- Postcard.

"EXPRESS MAIL" Mailing Label Number EL245467840US

Date of Deposit April 20, 1999  
I hereby certify under 37 CFR 1.10 that this correspondence is being deposited with the United States Postal Service as "Express Mail Post Office To Addressee" with sufficient postage on the date indicated above and is addressed to the Assistant Commissioner for Patents, Washington, D.C. 20231.

Kristy Cioffi  
Kristy Cioffi

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FISH & RICHARDSON P.C.

COPY

April 20, 1999

Page 2

Basic filing fee	760.00
Total claims in excess of 20 times \$18.00	576.00
Independent claims in excess of 3 times \$78.00	468.00
Fee for multiple dependent claims	0.00
Total filing fee:	\$ 1,804.00

A check for the filing fee is enclosed. Please apply any other required fees or any credits to deposit account 06-1050, referencing the attorney docket number shown above.

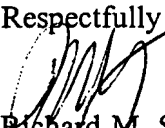
If this application is found to be incomplete, or if a telephone conference would otherwise be helpful, please call the undersigned at 617/542-5070.

Kindly acknowledge receipt of this application by returning the enclosed postcard.

Please send all correspondence to:

Richard M. Sharkansky  
Fish & Richardson P.C.  
225 Franklin Street  
Boston, MA 02110-2804

Respectfully submitted,

  
Richard M. Sharkansky  
Reg. No. 25,800  
Enclosures

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APPENDIX 1  
FOR APPLICATION

FOR

UNITED STATES LETTERS PATENT

TITLE: PREDICTING PERFORMANCE OF TELEPHONE LINES FOR  
DATA SERVICES

APPLICANT: KURT E. SCHMIDT, DAVID J. GROESSL AND YUN ZHANG

"EXPRESS MAIL" Mailing Label Number EL245467840US

Date of Deposit April 20, 1999

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Kristy Cioffi

Kristy Cioffi

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## Appendix 1

$f$ :

150, 600, 1050, 1500, 1950, 2400, 2850, 3300, 3750, 4200, 4650, 5100, 5550, 6000, 6450, 6900, 7350, 7800, 8250, 8700, 9150, 9600, 10050, 10500, 10950, 11400, 11850, 12300, 12750, 13200, 13650, 14100, 14550, 15000, 15450, 15900, 16350, 16800, 17250, 17700, 18150, 18600, 19050, 19500, 19950.

$N$ :

1, 4, 7, 10, 13, 16, 19, 22, 25, 28, 31, 34, 37, 40, 43, 46, 49, 52, 55, 58, 61, 64, 67, 70, 73, 76, 79, 82, 85, 88, 91, 94, 97, 100, 103, 106, 109, 112, 115, 118, 121, 124, 127, 130, 133 respectively.

$\varphi$ :

5.9738, 1.3564, 2.4683, 4.8575, 4.7424, 2.2972, 4.6015, 1.9156, 2.5660, 4.5986, 4.6452, 3.4542, 3.6341, 0.8848, 4.3410, 2.1606, 4.2342, 4.2147, 3.1058, 5.9049, 5.2782, 5.1159, 5.4354, 5.6124, 0.5751, 3.8940, 3.3812, 6.0230, 2.3239, 2.7284, 4.8032, 4.1488, 2.3427, 4.6362, 0.9163, 2.9335, 1.0363, 2.3272, 3.2040, 4.0025, 2.0028, 5.8444, 2.4525, 1.4760, 1.1770

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**APPENDIX 2  
FOR APPLICATION**

**FOR**

**UNITED STATES LETTERS PATENT**

**TITLE: PREDICTING PERFORMANCE OF TELEPHONE LINES FOR  
DATA SERVICES**

**APPLICANT: KURT E. SCHMIDT, DAVID J. GROESSL AND YUN ZHANG**

"EXPRESS MAIL" Mailing Label Number EL245467840US

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indicated above and is addressed to the Assistant Commissioner for  
Patents, Washington, D.C. 20231.

Kristy Cioffi  
Kristy Cioffi

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## Appendix 2

### 30Hz Raw Measurements:

Ytr(30) - Admittance tip-to-ring measured at 30Hz  
Ytg(30) - Admittance tip-to-ground measured at 30Hz  
Yrg(30) - Admittance ring-to-ground measured at 30Hz

### 30Hz Derived Measurements:

30Gtr - Conductance tip-to-ring measured at 30Hz =  $\text{real}(\text{Ytr}(30))$   
30Str - Susceptance tip-to-ring measured at 30Hz =  $\text{imag}(\text{Ytr}(30))$   
30Gtg - Conductance tip-to-ground measured at 30Hz =  $\text{real}(\text{Ytg}(30))$   
30Stg - Susceptance tip-to-ground measured at 30Hz =  $\text{imag}(\text{Ytg}(30))$   
30Ctr - Capacitance tip-to-ring measured at 30Hz =  $\text{Str}(30) / (2 \cdot \pi \cdot 30)$   
30Ctg - Capacitance tip-to-ground measured at 30Hz =  $\text{Stg}(30) / (2 \cdot \pi \cdot 30)$   
Lmeas - Length in kft measured at 30Hz =  $30\text{Ctg} / 17.47$

### 150Hz-20KHz Raw Measurements:

Ytr(f) - Admittance tip-to-ring where  $f=150\text{Hz}, 600\text{Hz}, 1050\text{Hz}, 1500\text{Hz}, \dots, 19950\text{Hz}$   
Ytg(f) - Admittance tip-to-ground where  $f=150\text{Hz}, 600\text{Hz}, 1050\text{Hz}, 1500\text{Hz}, \dots, 19950\text{Hz}$   
Yrg(f) - Admittance ring-to-ground where  $f=150\text{Hz}, 600\text{Hz}, 1050\text{Hz}, 1500\text{Hz}, \dots, 19950\text{Hz}$

### 150Hz-20KHz Derived Measurements:

150Gtr - Conductance tip-to-ring measured at 150Hz =  $\text{real}(\text{Ytr}(150))$   
600Gtr - Conductance tip-to-ring measured at 600Hz =  $\text{real}(\text{Ytr}(600))$   
  
19950Gtr - Conductance tip-to-ring measured at 19950Hz =  $\text{real}(\text{Ytr}(19950))$   
  
150Str - Susceptance tip-to-ring measured at 150Hz =  $\text{imag}(\text{Ytr}(150))$   
600Str - Susceptance tip-to-ring measured at 600Hz =  $\text{imag}(\text{Ytr}(600))$   
  
19950Str - Susceptance tip-to-ring measured at 19950Hz =  $\text{imag}(\text{Ytr}(19950))$   
  
150Gtg - Conductance tip-to-ground measured at 150Hz =  $\text{real}(\text{Ytg}(150))$   
600Gtg - Conductance tip-to-ground measured at 600Hz =  $\text{real}(\text{Ytg}(600))$   
  
19950Gtg - Conductance tip-to-ground measured at 19950Hz =  $\text{real}(\text{Ytg}(19950))$   
  
150Stg - Susceptance tip-to-ground measured at 150Hz =  $\text{imag}(\text{Ytg}(150))$   
600Stg - Susceptance tip-to-ground measured at 600Hz =  $\text{imag}(\text{Ytg}(600))$   
  
19950Stg - Susceptance tip-to-ground measured at 19950Hz =  $\text{imag}(\text{Ytg}(19950))$   
  
150Ctr - Capacitance tip-to-ring measured at 150Hz =  $150\text{Str} / (2 \cdot \pi \cdot 150)$   
600Ctr - Capacitance tip-to-ring measured at 600Hz =  $600\text{Str} / (2 \cdot \pi \cdot 600)$   
  
19950Ctr - Capacitance tip-to-ring measured at 19950Hz =  $19950\text{Str} / (2 \cdot \pi \cdot 19950)$   
  
150Ctg - Capacitance tip-to-ground measured at 150Hz =  $150\text{Stg} / (2 \cdot \pi \cdot 150)$   
600Ctg - Capacitance tip-to-ground measured at 600Hz =  $600\text{Stg} / (2 \cdot \pi \cdot 600)$   
  
19950Ctg - Capacitance tip-to-ground measured at 19950Hz =  $19950\text{Stg} / (2 \cdot \pi \cdot 19950)$

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## 150Hz-20KHz Secondary Derived Measurements:

C30/C4K - Ratio of tip-to-ground Capacitance at 30Hz to 4200Hz  
C4K/C10K - Ratio of tip-to-ground Capacitance at 4200Hz to 10050Hz  
Cslope - Tip-to-ground Capacitance ratio slope =  $(C4K/C10K)/(C30/C4K)$   
C30-C4K - Difference in tip-to-ground Capacitance at 30Hz and 4200Hz  
C4K-C10K - Difference in tip-to-ground Capacitance at 4200Hz and 10050Hz  
Cdelta - Tip-to-ground Capacitance difference delta =  $(C4K-C10K)/(C30-C4K)$

G4K/G30 - Ratio of tip-to-ground Conductance at 4200Hz to 30Hz  
G10K/G4K - Ratio of tip-to-ground Conductance at 10050Hz to 4200Hz  
Gslope - Tip-to-ground Conductance ratio slope =  $(G10K/G4K)/(G4K/G30)$   
G4K-G30 - Difference in tip-to-ground Conductance at 30Hz and 4200Hz  
G10K-G4K - Difference in tip-to-ground Conductance at 4200Hz and 10050Hz  
Gdelta - Tip-to-ground Conductance difference delta =  $(G10K-G4K)/(G4K-G30)$

C30/G30 - Ratio of Tip-to-ground Capacitance to Conductance at 30Hz  
C30/G4K - Ratio of Tip-to-ground Capacitance at 30Hz to Conductance at 4200Hz  
C4K/G4K - Ratio of Tip-to-ground Capacitance to Conductance at 4200Hz

Gtr\_dmax - Maximum positive slope of  $Gtr(f) = \max(\text{derivative}(Gtr(f)/df))$   
Gtr\_fmax - Frequency at which Gtr\_dmax occurs  
Gtr\_dmin - Maximum negative slope of  $Gtr(f) = \min(\text{derivative}(Gtr(f)/df))$   
Gtr\_fmin - Frequency at which Gtr\_dmin occurs  
Gtr\_fpk - Frequency of first peak (local maxima) in  $Gtr(f)$   
Gtr\_fval - Frequency of first valley (local minima) in  $Gtr(f)$   
Gtr\_d\_delta - Gtr Max/Min Derivative difference =  $Gtr\_dmax - Gtr\_dmin$   
Gtr\_pk\_delta - Gtr peak/valley frequency difference =  $Gtr\_fval - Gtr\_fpk$   
Gtr\_pk - Value of  $Gtr(f)$  at frequency  $Gtr\_fpk$   
Gtr\_val - Value of  $Gtr(f)$  at frequency  $Gtr\_fval$   
Gtr\_delta - Gtr peak/valley difference =  $Gtr\_pk - Gtr\_val$

Gtg\_dmax - Maximum positive slope of  $Gtg(f) = \max(\text{derivative}(Gtg(f)/df))$   
Gtg\_fmax - Frequency at which Gtg\_dmax occurs  
Gtg\_dmin - Maximum negative slope of  $Gtg(f) = \min(\text{derivative}(Gtg(f)/df))$   
Gtg\_fmin - Frequency at which Gtg\_dmin occurs  
Gtg\_d\_delta - Gtg Max/Min Derivative difference =  $Gtg\_dmax - Gtg\_dmin$

Ctr\_dmax - Maximum positive slope of  $Ctr(f) = \max(\text{derivative}(Ctr(f)/df))$   
Ctr\_fmax - Frequency at which Ctr\_dmax occurs  
Ctr\_dmin - Maximum negative slope of  $Ctr(f) = \min(\text{derivative}(Ctr(f)/df))$   
Ctr\_fmin - Frequency at which Ctr\_dmin occurs  
Ctr\_fpk - Frequency of first peak (local maxima) in  $Ctr(f)$   
Ctr\_fval - Frequency of first valley (local minima) in  $Ctr(f)$   
Ctr\_d\_delta - Ctr Max/Min Derivative difference =  $Ctr\_dmax - Ctr\_dmin$   
Ctr\_pk\_delta - Ctr peak/valley frequency difference =  $Ctr\_fval - Ctr\_fpk$   
Ctr\_val - Value of  $Ctr(f)$  at frequency  $Ctr\_fval$

Ctg\_dmax - Maximum positive slope of  $Ctg(f) = \max(\text{derivative}(Ctg(f)/df))$   
Ctg\_fmax - Frequency at which Ctg\_dmax occurs  
Ctg\_dmin - Maximum negative slope of  $Ctg(f) = \min(\text{derivative}(Ctg(f)/df))$   
Ctg\_fmin - Frequency at which Ctg\_dmin occurs  
Ctg\_d\_delta - Ctg Max/Min Derivative difference =  $Ctg\_dmax - Ctg\_dmin$

Str\_dmax - Maximum positive slope of  $Str(f) = \max(\text{derivative}(Str(f)/df))$   
Str\_fmax - Frequency at which Str\_dmax occurs  
Str\_dmin - Maximum negative slope of  $Str(f) = \min(\text{derivative}(Str(f)/df))$   
Str\_fmin - Frequency at which Str\_dmin occurs

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## 150Hz-20KHz Secondary Derived Measurements:

Str\_fpk - Frequency of first peak (local maxima) in Str(f)  
Str\_fval - Frequency of first valley (local minima) in Str(f)  
Str\_d\_delta - Str Max/Min Derivative difference = Str\_dmax-Str\_dmin  
Str\_pk\_delta - Str peak/valley frequency difference = Str\_fval-Str\_fpk  
Str\_pk - Value of Str(f) at frequency Str\_fpk  
Str\_val - Value of Str(f) at frequency Str\_fval  
Str\_delta - Str peak/valley difference = Str\_pk-Str\_val

Stg\_dmax - Maximum positive slope of Stg(f) = max(derivative(Stg(f)/df))  
Stg\_fmax - Frequency at which Stg\_dmax occurs  
Stg\_dmin - Maximum negative slope of Stg(f) = min(derivative(Stg(f)/df))  
Stg\_fmin - Frequency at which Stg\_dmin occurs  
Stg\_fpk - Frequency of first peak (local maxima) in Stg(f)  
Stg\_fval - Frequency of first valley (local minima) in Stg(f)  
Stg\_d\_delta - Stg Max/Min Derivative difference = Stg\_dmax-Stg\_dmin  
Stg\_pk\_delta - Stg peak/valley frequency difference = Stg\_fval-Stg\_fpk

Gtg20k/Gtg8k - Ratio of Gtg at 19950Hz and 8250Hz  
Gtg20k/Gtg4k - Ratio of Gtg at 19950Hz and 4200Hz  
Cgt30/Cgt20k - Ratio of Ctg at 30Hz and 19950Hz  
Cgt30/Cgt8k - Ratio of Ctg at 30Hz and 8250Hz